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### Dual technology energy storage system applied to two complementary electricity markets using a weekly differentiated approach

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#### Abstract

This paper deals with integration of energy storage systems into electricity markets. We explain why the energy storage systems increase flexibility of both power systems and energy markets and why such flexibility is desirable, particularly when variable renewable energy sources are being used in existing power systems. As opposed to the existing literature, our model includes a dual technology energy storage system, acting in two different markets. We introduce a mathematical formulation for this model applied to two Dutch electricity markets. Adopting optimal control approach with the goal to maximize the yearly benefit, we show that the dual energy storage system can be profitable already when the same buying/selling strategies are adopted for the working days and weekends. We show that the profitability (slightly) increases with different buying/selling strategies for the weekdays and weekends. Finally, we demonstrate how the yearly benefit varies with

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size and efficiency of the devices chosen and market prices.

*Keywords:* Energy Storage Systems, Electricity Markets, Renewable Energy Sources Integration, Optimal Control, Optimization

#### 1 1. INTRODUCTION

#### <sup>2</sup> 1.1. Motivation, Background and Literature Review

The worldwide energy policy goals include further integration of the renewable generation technologies into the energy markets. For example, the European Union is striving to achieve 20% of energy generated from re-5 newable energy sources (RES) by 2020 and to reach a minimum of 27% of 6 renewable generated energy by 2030, while reducing greenhouse gas emis-7 sions by at least 40% by 2030 compared to their level in 1990 [1]. Objectives 8 for 2050 are even more challenging, with a reduction of the carbon emissions 9 by 80 - 95% [2]. All around the world (e.g. in China [3], Japan [4], New 10 Zealand [5], United States of America [6, 7] and Turkey [8]) the power sys-11 tems are being prepared for an increasing level of deployment of renewable 12 generation technologies. 13

In conjunction with RES, the integration of other recent technologies, 14 such as electric vehicles (EV), but also the unbundling and modification in 15 the regulation of the power sector, influence the paradigm and structure 16 of the power sector. As electricity has to be dealt with when generated, 17 either by being consumed or stored, matching the levels of generation and 18 load at all times is fundamental. The fact that most RES are weather-19 dependent will cause the generation output to vary more likely with the 20 climate conditions than with the market needs. The increasing integration 21 of electric vehicles also increases the likelihood of high load variations during 22 the day. The novel technologies are expected to be applied to an extent 23 which will certainly amplify the effect of these variations. 24

The above mentioned technological and regulatory developments call for adjustment of planning and operation of the power systems – they need to be more flexible. This flexibility can be achieved through several technologies and techniques (e.g. energy storage systems (ESSs'), cross-border interconnection capacity, RES management, more flexibility from conventional generation, active demand side management and vehicle-to-grid) and their combinations [9]. Among these, ESS is seen as one of the long term most feasible options to achieve that goal [10].

ESSs can provide up to twice their rating (sum of charge and discharge capacities) to balance the electricity grid. This is accomplished by switching between the two modes of charging and discharging, in either direction (from charging to discharging or from discharging to charging). Therefore, ESSs help to balance the electricity system when there is a generation surplus or a deficit. ESSs can provide various services, most important of which belong to one of the two major categories:

40 i. power market arbitrage

<sup>41</sup> ii. ancillary services and balancing

Power market arbitrage is an energy service provided via charging an en-42 ergy storage device when the electricity prices are low and discharging it 43 when the prices are high [11]. The price variations are caused by daily, 44 weekly or seasonal cycles. Lately, also variations in renewable power gen-45 eration, e.g. wind and solar energy, are affecting the energy markets to a 46 degree depending on their level of market penetration and the flexibility of 47 the underlying conventional generation fleet. The most adequate markets 48 exercising arbitrage are day-ahead and intra-day markets [12]. 49

In unbundled markets, the system operators are not allowed to own energy generation assets. Therefore, they need to procure several ancillary services. Examples of these ancillary services are balancing support and congestion management.

Other services can be supplied by ESSs [6, 7, 11]. [11], depending on 54 the characteristics of the specific energy storage technologies. The problem 55 of energy storage integration into existing electricity markets was studied 56 in [13, 14, 15]. The literature implies that in most markets, with current 57 price differences, arbitrage provision is not sufficient to make energy storage 58 profitable. Hybrid energy storage systems using two energy storage devices 59 are present in the literature. However, these are associated with electric 60 vehicle power system or variable renewable energy generation site integration 61 into the grid [16]. Nonetheless, to the best of our knowledge, no models 62 including two electricity markets and two ESS technologies operating in 63 parallel have been developed so far. 64

This paper focuses on a combination of energy market arbitrage and provision of balancing support by the same dual energy storage system. The

model that we introduce in this paper differs from the models analysed in 67 the literature in two major aspects. Firstly, we consider a system combining 68 arbitrage and ancillary services. With this combination we expect higher 69 yearly benefits than using arbitrage only. Secondly, the energy storage sys-70 tem that we propose uses two energy storage technologies simultaneously. 71 The dual technology system was chosen in order to profit from character-72 istics of both devices and market price variations. This paper extends our 73 research presented in [17]. 74

In order to see how profitable the ESS could be, in this paper we seek op-75 timal strategy in terms of price thresholds for buying and selling electricity at 76 the Dutch day-ahead and balancing electricity markets. Mathematically, we 77 formulate the problem as an optimal control problem with the goal to max-78 imize the yearly benefit. Firstly, we consider the situation when buying and 79 selling thresholds may vary between working days and weekends. Secondly, 80 we consider a situation when the working days and weekend thresholds are 81 the same. We use pattern search to find the optimal strategy and motivate 82 the choice of this method. 83

The remainder of this paper is composed as follows. Section 2 introduces electricity markets in The Netherlands. Section 3 explains the background of the model we put forward. The problem dealt within this paper is defined mathematically in Section 4. Implementation of the model and a solution method are described in Section 5. Section 6 presents and discusses the results of the case studies. Section 7 finalizes the paper with the conclusions and directions for future research.

#### 91 1.2. Notation

Table 1 describes the main symbols used in this paper.

Symbol	Description	Unit
J	set of electricity markets and of energy storage devices, $J = \{1, 2\}$	
j	electricity market/storage device, element of set $J$	
D	set of days under analysis	
δ	day, element of set $D$	
$T_j$	set of time steps for market $j$ within a day <sup>‡</sup>	
$t_j$	element of $T_j$ ; time step for market $j$ within a day	
$M^{j}$	set of possible modes for market $j$ , $M^1 = \{0\}$ , $M^2 = \{-1, 0, 1, 2\}$	
$m^{j,\delta,t_j}$	mode of market j on day $\delta$ and time step $t_j$ , element of set $M^j$	
$k(\delta)$	day type; indication of working days/weekends, $k(\delta) \in \{1, 2\}$	
$h^{j,k(\delta)}$	relative buying threshold for market $j$	
$n_B$	and day type $k(\delta), h_B^{j,k(\delta)} \in [0,1]$	
$_{k}j,k(\delta)$	relative selling threshold for market $j$	
$n_S$	and day type $k(\delta), h_S^{j,k(\delta)} \in [0,1]$	
u	vector of buying and selling price thresholds (to be optimized)	
Z(u)	yearly benefit	
$\Sigma(u)$	when set of thresholds $u$ is adopted	€
au*	vector of optimal buying and selling price thresholds	
u	maximizing $Z(u)$	
$j, \delta, t_j, m^{j, \delta, t_j}$	energy quantity sold in market $j$ ,	
$q_S$	mode $m^{j,\delta,t_j}$ , day $\delta$ and time step $t_j$	MWh
$\alpha^{j,\delta,t_j,m^{j,\delta,t_j}}$	energy quantity bought in market $j$ ,	
$q_B$	mode $m^{j,\delta,t_j}$ , day $\delta$ and time step $t_j$	MWh
$m^{j,\delta,t_j,m^{j,\delta,t_j}}$	selling energy price in market $j$ ,	- /
$p_S$	mode $m^{j,o,\iota_j}$ , day $\delta$ and time step $t_j$	€/MWh
$m^{j,\delta,t_j,m^{j,\delta,t_j}}$	buying energy price in market $j$ ,	
$\frac{P_B}{\delta}$	day $\delta$ , time step $t_j$ and mode $m^{j,\delta,t_j}$	€/MWh
$\frac{\pi_B^{J,0}}{1}$	minimum buying price for market $j$ on day $\delta$	€/MWh
$\pi_S^{j,o}$	minimum selling price for market $j$ on day $\delta$	€/MWh
$x^{j,\delta,t_j,m^{j,\delta,t_j}}$	state of charge of device $j$ on day $\delta$ , time step $t_j$ and mode $m^{j,\delta,t_j}$	MWh
$j, \delta, t_j, m^{j, \delta, t_j}$	quantity of energy discharged by device $j$ ,	
$q_D$ ,	on day $\delta$ , time step $t_j$ and mode $m^{j,\delta,t_j}$	MWh
$j, \delta, t_j, m^{j, \delta, t_j}$	quantity of energy charged by device $j$ ,	
$q_C$	on day $\delta$ , time step $t_j$ and mode $m^{j,\delta,t_j}$	MWh
$\eta_D^j$	discharging efficiency of device $j, \eta_D^j \in [0, 1]$	
$\eta_C^j$	charging efficiency of device $j, \eta_C^j \in [0, 1]$	
$q_{C,\max}^j$	maximum amount of energy that	
	device $j$ can charge in one time step	MWh
$a_{\rm D}^j$	maximum amount of energy that	
4D,max	device $j$ can discharge in one time step	MWh
$x_{\min}^j$	minimum state of charge of device $j$	MWh
$x_{\max}^j$	maximum state of charge of device $j$	MWh

Table 1: Main symbols used in this paper, their meaning, and units (if applicable)

<sup>‡</sup> typical values: 24 time units for an hourly market, 96 time units for market with quarters of hour as a basic time unit

Symbol	Description	Unit	
$\lambda^{2,\delta,t_2,m^{2,\delta,t_2}}$	energy received by device 2, transferred from		
	device 1, on day $\delta$ , time step $t_2$ and mode $m^{2,\delta,t_2}$	MWh	
$\gamma^{1,\delta,t_1,m^{1,\delta,t_1}}$	energy reserved by device 1 to be transferred		
	to device 2 on day $\delta$ , time step $t_1$ and mode $m^{1,\delta,t_1}$	MWh	
$(1, \delta, t_1, m^{1, \delta, t_1})$	energy reserved on device 1 and not used to		
$\phi$	supply device 2 on day $\delta$ , time step $t_1$ and mode $m^{1,\delta,t_1}$	MWh	
$\sigma^{j,\delta}$	historical price volatility in market $j$ for day $\delta$		
$t_{j-t_{j-1}}$	and time difference $t_j - t_{j-1}$		
	price return,		
$v_{t_{i}-t_{i-1}}^{j,o,\iota_{j}}$	ratio between prices at time step $t_j$ and		
	at time step $t_{j-1}$ , for market j and day $\delta$		
$\overline{v}^{j,\delta}$	mean price return in market $j$ , day $\delta$		
a/j	minimum payback period		
Ψ	for the technology $j$ under analysis	years	
$\rho^j$	power rating of device $j$	kW	
$\mu^j$	cost per unit of power of device $j$	€/kW	
$\epsilon^{j}$	energy rating of device $j$	kW	
$\xi^{j}$	cost per unit of energy of device $j$	€/kWh	
o <sup>j</sup>	yearly fixed operation	£	
	and maintenance costs for device $j$	Ð	
$\kappa^{j}$	variable operation and maintenance	∉/kWh	
	costs for device $j$		
ι	internal rate of return	%	

Table 2: Main symbols used in this paper, their meaning, and units (if applicable), continuation of Table 1  $\,$ 

\* Please check note ‡ in Table 1.

#### 93 2. Electricity Markets in The Netherlands

In The Netherlands most of the electricity is still traded in the bilat-94 eral market, where the generation companies sell the electricity directly to 95 large consumers, traders and supply companies. The remaining electricity 96 generated is traded in one of the two spot markets: the day-ahead and 97 intra-day markets. For balancing purposes also a dedicated market exists, 98 managed by the Dutch transmission system operator (TSO) TenneT. The 99 day-ahead and intra-day markets have distinct dimensions. For 2011, about 100 40 TWh of electricity were traded in the day-ahead market and less than 101 1% of that value, 278 GWh, were traded in the intra-day market [19]. The 102 Netherlands has been identified as "the most promising [electricity market] 103 for mass storage" [18]. 104

#### 105 2.1. Day-ahead market

The Dutch day-ahead market is active every day prior to the day of 106 operation and closes at noon. This market has an hourly time unit. Unless 107 stated differently, in this paper we use price data from 2014. For this year, 108 we calculated the mean price of energy per MWh for the Dutch day-ahead 109 market:  $41.18 \in MWh$ . Figure 1 depicts the average prices for 2014 and 110 both day-ahead and balancing market. It is possible to observe the weekend 111 variation in the day-ahead market in the last two days, where prices tend 112 to be lower than during the weekdays. 113

#### 114 2.2. Balancing market

Balancing markets are volatile, and are used to balance the unattended 115 mismatch between generation and load. In The Netherlands, the balan-116 cing market, also called imbalance market, works with a time unit of 15 117 minutes. This unit is also called program time unit (PTU). This market is 118 managed by TenneT, the national transmission system operator (TSO). The 119 TSO tries to avoid the mismatch mentioned as much as possible by sharing 120 balancing responsibilities with balancing responsible parties (BRPs). Each 121 BRP aggregates a part of the consumers and generators in the network. The 122 BRPs submit their daily zero-sum comsumption and generation plans ex-123 ante. Each of these plans include their expected net energy exchange with 124 the other BRPs to the TSO. Afterwards, in real time, the TSO verifies if 125 there is any imbalance in the system. 126

There are two types of BRPs, those specifically asked to provide balancing capacity by active contributions (Balancing Service Providers - BSPs) and those either using the imbalance settlement system for their own imbalance or being active without being selected [20]. By bidding on the imbalance market, each BRP gives the TSO the right (but not the obligation) to buy balancing energy.

Load forecasting is not exact and energy generation forecasting with increasing integration of variable renewable-based generation is harder to achieve. Thus, the balancing market is used to solve these unexpected variations, by trading flexibility. Traditionally, this was achieved by increasing or decreasing generation [21]. Recently, whenever available, also demand side response and energy storage may be used [21], as long as the technologies used can cope with the response time required by the system operator.

The Dutch imbalance market has 4 possible modes: downwards, upwards, 140 upwards/downwards and no contribution, which we will denote by -1, 1, 2141 and 0, respectively (see Table 3). These modes are calculated by the TSO 142 in the real time. In mode -1 there is an excess of power in the system. This 143 excess of power is also called "long" and requires downward regulation. In 144 mode 1 there is a lack of power in the system. This lack of power is also 145 called "short" and requires upward regulation. In mode 2 there are periods 146 of both excess and lack of power in the system within the time step of 15 147 minutes, while in mode 0 there is no imbalance. 148





Table 3: Balancing modes in The Netherlands, based on [20]				
Balancing mode $(m^{2,\delta,t_2})$	-1	0	1	2
Condition	Long (Downward)	No Imbalance	Short (Upward)	Both long and short

Based on data from 2014, we calculated the average price of energy per MWh for the Dutch balancing market: for upward regulation (mode 1) it is  $38.31 \in /MWh$  and for downward regulation (mode -1) it is  $11.12 \in /MWh$ . The prices in this market vary during the week as shown in Figure 1. Figure 2 shows the frequency of 2014 prices for both day-ahead and balancing markets (upward and downward). The two figures suggest that the prices vary more in the balancing market than in the day-ahead market.



Figure 2: Price histogram for the day-ahead market prices and balancing market upward and downward prices for 2014. Each bin has a range size of  $2 \in$ .

As the yearly benefit of the dual energy storage system depends on the price fluctuations in both markets, we have calculated the historical price volatility of the prices, which is a measure of price fluctuations observed
over a given time period (e.g. hourly, daily, weekly or yearly) [21], see also
appendix B for details of its calculation. Figure 3 shows the 2014 price
volatility towards the previous time slot of the same day (one hour in the
day ahead market and one PTU in the balancing market) for the three types
of prices of the two markets. Clearly, the balancing market is more volatile
than the day-ahead market



Figure 3: Volatility towards previous time slot (hour or PTU, depending on the market) for the 2014 day-ahead and balancing market prices.

164

#### 165 3. Model Background

In this section we introduce the background of our model. The two energy
storage technologies considered are a high energy (bulk) and a high power
technology, trading in the day-ahead and balancing markets, respectively.

The model is built from the point of view of the owner of the energy storage system, with the goal of maximizing the yearly benefit. The dayahead market is used to perform energy price arbitrage and the balancingmarket is used to provide ancillary service support.

Figure 4 depicts the relationship between the considered markets and
the two types of energy storage devices. We have built two submodels, each
of them describing the behaviour of one of these devices (see Section 5 for details).



Figure 4: Illustration of the relationship between the considered energy markets and energy storage devices. The arrows indicate the possible energy transfer directions. The numbers 1 and 2 identify the two submodels.

176

For the sake of simplicity, in our model we assume both perfect electricity price forecast and a price taker approach, based on two assumptions:

179 1. The storage size is not big enough to modify market prices [23].

2. There is a perfect forecast window, more or less extended according
to the study [23].

These two assumptions are very standard when analysing potential profitability of energy storage systems in a modeling framework.

#### 184 4. Model Formulation

Our goal is to find the optimal charge and discharge relative price bound-185 aries, per device type and day, so that the yearly benefit obtained is maxim-186 ized. Mathematically speaking, the problem of finding the optimal strategy 187 for the energy storage system operation, composed of the finite set J of 188 storage devices, can be formulated as an optimal control problem. For the 189 sake of simplicity, we assume that each device has a unique type and that 190 this type uniquely identifies the type of market it is used for.<sup>1</sup> This paper 191 considers  $J = \{1, 2\}$ , where j = 1 identifies both Dutch day-ahead electricity 192 market and bulk energy storage device, while j = 2 identifies both Dutch 193 balancing electricity market and high power energy storage device. For cla-194 rification on the meaning of the main variables used in our model, please 195 see Table 1. 196

Mathematical formulation of the optimal control problem dealt with in this paper reads as follows:

$$u^* = \arg\max_{u \in U} Z(u), \tag{1}$$

where the yearly benefit Z(u) for the vector of relative price thresholds  $u = (h_B^{1,1}, h_S^{1,1}, ..., h_B^{2,2}, h_S^{2,2})$  is defined as

$$\sum_{j\in J}\sum_{\delta\in D}\sum_{t_j\in T_j}\sum_{m^{j,\delta,t_j}\in M^j} \left(q_S^{j,\delta,t_j,m^{j,\delta,t_j}} \cdot p_S^{j,\delta,t_j,m^{j,\delta,t_j}} - q_B^{j,\delta,t_j,m^{j,\delta,t_j}} \cdot p_B^{j,\delta,t_j,m^{j,\delta,t_j}}\right),$$
(2)

with respect to equations (3) –(26). Here  $U = ([0,1])^{2 \cdot n_K \cdot n_J}$  and  $h_B^{j,k(\delta)}$  and  $h_S^{j,k(\delta)}$  refer to relative buying and selling thresholds prices, respectively. The actual buying and selling prices  $\pi_B^{j,\delta}$  and  $\pi_S^{j,\delta}$  can be then calculated as

 $<sup>^1\</sup>mathrm{However},$  this assumption does not change the main ideas behind the model and can be easily relaxed.

follows:

$$\pi_B^{j,\delta} = \frac{\sum_{t_j \in T_j} \sum_{m^{j,\delta,t_j \in M^j}} p_B^{j,\delta,t_j,m^{j,\delta,t_j}}}{n_{T_j}^{m^{j,\delta,t_j}}} \cdot (1 - h_B^{j,k(\delta)}),$$
(3)

$$\pi_{S}^{j,\delta} = \frac{\sum_{t_{j}\in T_{j}} \sum_{m^{j,\delta,t_{j}\in M^{j}}} p_{S}^{j,\delta,t_{j},m^{j,\delta,t_{j}}}}{n_{T_{j}}^{m^{j,\delta,t_{j}}}} \cdot (1+h_{S}^{j,k(\delta)}), \qquad (4)$$
where  $k(\delta) = \begin{cases} 1, & \text{if } \mod(\delta,7) \in \{1,2,3,4,5\},\\ 2, & \text{otherwise.} \end{cases}$ 

Market 1 is always in the same mode 0, i.e.,  $M^1 = 0$ , while  $M^2 = \{-1, 0, 1, 2\}$  (see Table 3 for overview of these modes). In mode  $m^{2,\delta,t_2} = 2$  only one action (buying or selling) is allowed for device 2. We assume that in such a situation device 2 sells, because selling is more advantageous for the energy storage owner, as shown in [17]. Due to the efficiency losses in charging and discharging, one has to buy more electricity than it can be physically charged into a device and, similarly, one has to discharge more electricity than the amount of energy sold:

$$q_B^{j,\delta,t_j,m^{j,\delta,t_j}} = \frac{q_C^{j,\delta,t_j,m^{j,\delta,t_j}}}{\eta_C^j}, \quad q_S^{j,\delta,t_j,m^{j,\delta,t_j}} = q_D^{j,\delta,t_j,m^{j,\delta,t_j}} \cdot \eta_D^j, \tag{5}$$

where  $\eta_D^j \in [0, 1]$  and  $\eta_C^j \in [0, 1]$  refer to the efficiencies of discharging and charging, respectively, and are known a priori.

. . .

No device can simultaneously charge and discharge electricity and the amount of electricity charged and discharged cannot exceed its prespecified boundaries, i.e.,

$$q_{C}^{j,\delta,t_{j},m^{j,\delta,t_{j}}} \cdot q_{D}^{j,\delta,t_{j},m^{j,\delta,t_{j}}} = 0, \quad q_{C}^{j,\delta,t_{j},m^{j,\delta,t_{j}}} \in [0, q_{C,\max}^{j}],$$

$$q_{D}^{j,\delta,t_{j},m^{j,\delta,t_{j}}} \in [0, q_{D,\max}^{j}].$$
(6)

As each market/device j can only be in one mode  $m^{j,\delta,t_j}$  on day  $\delta$  and time step  $t_j$ , we set quantities of electricity charged and discharged and their buying and selling prices for all other but the current mode, same day  $\delta$  and time step  $t_j$ , to zero:

$$q_C^{j,\delta,t_j,b} = 0 \quad \forall b \in M^j \setminus \{m^{j,\delta,t_j}\}, \quad \text{if} \quad q_C^{j,\delta,t_j,m^{j,\delta,t_j}} > 0, \tag{7}$$

$$q_D^{j,\delta,t_j,b} = 0 \quad \forall b \in M^j \setminus \{m^{j,\delta,t_j}\}, \quad \text{if} \quad q_D^{j,\delta,t_j,m^{j,\delta,t_j}} > 0, \tag{8}$$

$$p_B^{j,\delta,t_j,b} = 0 \quad \forall b \in M^j \setminus \{m^{j,\delta,t_j}\}, \quad \text{if} \quad p_B^{j,\delta,t_j,m^{j,\delta,t_j}} > 0, \tag{9}$$

$$p_S^{j,\delta,t_j,b} = 0 \quad \forall b \in M^j \setminus \{m^{j,\delta,t_j}\}, \quad \text{if} \quad p_S^{j,\delta,t_j,m^{j,o,i_j}} > 0.$$
(10)

<sup>199</sup> Mode  $m^{j,\delta,t_j}$  and electricity prices for each market j, day  $\delta$  and time step  $t_j$ <sup>200</sup> are exogenous and assumed to be known *a priori*.

Our model takes advantage of any lower prices in the day-ahead market when compared with the balancing market, by transferring energy from device 1 to device 2. As device 2 has a time step of 15 minutes, two complete cycles of charging and discharging may be performed in one hour.

In order to avoid any inconsistency, since device 1 and device 2 are used in our model with different time steps, the energy transferable from one device to another is reserved *a priori*. This reservation is performed every hour, which is the time step of device 1 and larger of the two time steps. Equation (11) determines this energy reserved in device 1 transferable to device 2. As device 1 is much bigger than device 2, device 1 can provide a temporary additional output to charge device 2 when needed:

$$\gamma^{1,\delta,t_1,m^{1,\delta,t_1}} = \begin{cases} \frac{2 \cdot q_{C,\max}^2}{\eta_D^1 \cdot \eta_C^2}, \text{ if } x^{1,\delta,t_1-1,m^{1,\delta,t_1-1}} + q_C^{1,\delta,t_1,m^{1,\delta,t_1}} \\ & \geq \frac{2 \cdot q_{C,\max}^2}{\eta_D^1 \cdot \eta_C^2} + x_{\min}^1, \\ 0, \text{ otherwise.} \end{cases}$$
(11)

The energy transfer will only happen when device 2 is not being used in market 2 in the current time step  $t_2$ , as stated in (12). Also, device 2 can only receive energy if it is partially or fully discharged. If so, device 2 will receive the energy from device 1 ( $\lambda^{2,\delta,t_2,m^{2,\delta,t_2}}$ ). This amount will be the lower of two values: maximum quantity  $q_{C,\max}^2$  charged by device 2 or the energy  $\frac{x^{1,\delta,t_1,m^{1,\delta,t_1}}-x_{\min}^1}{\eta_D^1\cdot\eta_C^2}$  that can be transferred to device 2 from device 1.

This transfer can occur in every 15 minutes. For each  $t_2 \in \{4t_1-3,\ldots,4t_1\}$ ,

$$\lambda^{2,\delta,t_2,m^{2,\delta,t_2}} = \begin{cases} \min(q_{C,\max}^2, x_{\max}^2 - x^{2,\delta,t_2-1,m^{2,\delta,t_2-1}}), \\ \text{if} & \gamma^{1,\delta,t_1,m^{1,\delta,t_1}} \neq 0, \\ q_C^{2,\delta,t_2,m^{2,\delta,t_2}} = 0 & (12) \\ \text{and} & q_D^{2,\delta,t_2,m^{2,\delta,t_2}} = 0, \\ 0, & \text{otherwise.} \end{cases}$$

The amount of energy reserved in device 1 not transferred to device 2 is defined as For each  $t_1 = 1, 2, ...$ 

$$\phi^{1,\delta,t_1+1,m^{1,\delta,t_1+1}} = \gamma^{1,\delta,t_1,m^{1,\delta,t_1}} - \frac{\sum_{i=1}^4 \lambda^{2,\delta,(t_1-1)\cdot 4+i,m^{2,\delta,(t_1-1)\cdot 4+i}}}{\eta_D^1 \cdot \eta_C^2}.$$
 (13)

Here also the losses of discharging device 1 and charging device 2 are taken into consideration. The current state of charge of devices 1 and 2 depends on their state of charge in the previous time step:

$$x^{1,\delta,t_1,m^{1,\delta,t_1}} = x^{1,\delta,t_1-1,m^{1,\delta,t_1-1}} + q_C^{1,\delta,t_1,m^{1,\delta,t_1}} - q_D^{1,\delta,t_1,m^{1,\delta,t_1}} - \gamma^{1,\delta,t_1,m^{1,\delta,t_1}} + \phi^{1,\delta,t_1,m^{1,\delta,t_1}},$$
(14)  
$$x^{2,\delta,t_2,m^{2,\delta,t_2}} = x^{2,\delta,t_2-1,m^{2,\delta,t_2-1}} + q_C^{2,\delta,t_2,m^{2,\delta,t_2}}$$

$$-q_D^{2,\delta,t_2,m^{2,\delta,t_2}} + \lambda^{2,\delta,t_2,m^{2,\delta,t_2}}.$$
(15)

When it is not possible to charge or discharge quantities  $q_{C,\max}^1$  or  $q_{D,\max}^1$ , the device will charge or discharge as much as possible, given by  $x_{\max}^1 - x^{1,\delta,t_1-1,m^{1,\delta,t_1-1}}$  and  $x^{1,\delta,t_1-1,m^{1,\delta,t_1-1}} - x_{\min}^1$ , respectively. As most energy storage devices cannot be fully discharged,  $x_{\min}^j$  represents the minimum useful state of charge, the lowest charge level the storage device can be discharged to. Quantity  $q_D^{1,m^{1,\delta,t_1,\delta,t_1}}$  is defined as follows:

$$q_D^{1,\delta,t_1,m^{1,\delta,t_1}} = \begin{cases} \min(q_{D,\max}^1, x^{1,\delta,t_1-1,m^{1,\delta,t_1-1}} - x_{\min}^1), \\ \text{and} \quad p_S^{1,\delta,t_1,m^{1,\delta,t_1}} \ge \pi_S^{1,\delta}, \\ 0, \quad \text{otherwise.} \end{cases}$$
(16)

As device 1 starts discharged, equation (16) is only valid for  $t_1 \ge 2$  or when  $\delta \ge 2$ . Likewise,  $q_C^{1,m^{1,\delta,t_1},\delta,t_1}$  is defined as follows:

$$q_{C}^{1,\delta,t_{1},m^{1,\delta,t_{1}}} = \begin{cases} \min(q_{C,\max}^{1}, x_{\max}^{1} - x^{1,\delta,t_{1}-1}, m^{1,\delta,t_{1}-1}), \\ \text{if } p_{B}^{1,\delta,t_{1},m^{1,\delta,t_{1}}} \leq \pi_{B}^{1,\delta}, \\ 0, \text{ otherwise.} \end{cases}$$
(17)

If device 2 cannot charge the maximum quantity of energy charged  $q_{C,\max}^2$ , as it would overrun the maximum amount of charge  $x_{\max}^2$ , it will charge quantity  $x_{\max}^2 - x^{2,\delta,t_2-1,m^{2,\delta,t_2-1}}$ . Similarly, when discharging, if device 2 cannot discharge the maximum quantity of energy discharged  $q_{D,\max}^2$ , as it would overrun the functional minimum amount of charge  $x_{\min}^2$ , it will charge the quantity  $x^{2,\delta,t_2-1,m^{2,\delta,t_2-1}} - x_{\min}^2$ .

$$q_D^{2,\delta,t_2,m^{2,\delta,t_2}} = \begin{cases} \min(q_{D,\max}^2, x^{2,\delta,t_2-1,m^{2,\delta,t_2-1}} - x_{\min}^2), \\ \text{if } m^{2,\delta,t_2} \in \{1,2\}, \\ p_S^{2,\delta,t_2,m^{2,\delta,t_2}} \ge \pi_S^{2,\delta}, \\ 0, \text{ otherwise.} \end{cases}$$
(18)

$$q_{C}^{2,\delta,t_{2},m^{2,\delta,t_{2}}} = \begin{cases} \min(q_{C,\max}^{2}, x_{\max}^{2} - x^{2,\delta,t_{2}-1,m^{2,\delta,t_{2}-1}}), \\ \text{if } m^{2,\delta,t_{2}} = -1, \\ \text{and } p_{B}^{2,\delta,t_{2},m^{2,\delta,t_{2}}} \leq \pi_{B}^{2,\delta}, \\ 0, \text{ otherwise.} \end{cases}$$
(19)

As device 2 starts discharged, equation (18) is only valid only for  $t_2 \ge 2$  or when  $\delta \ge 2$ .

The maximum discharge capacity  $q_{D,\max}^1$  of device 1 is lower or equal to its maximum state of charge  $x_{\max}^1$  minus the transferable energy to device 2  $\frac{2\cdot q_{C,\max}^2}{\eta_D^1\cdot \eta_C^2}$ :

$$q_{D,\max}^{1} \le x_{\max}^{1} - \frac{2 \cdot q_{C,\max}^{2}}{\eta_{D}^{1} \cdot \eta_{C}^{2}}.$$
 (20)

Other constraints:

$$q_{C,\max}^j \le x_{\max}^j,\tag{21}$$

$$q_{D,\max}^2 \le x_{\max}^2,\tag{22}$$

$$q_{D,\min}^{j} = q_{C,\min}^{j} = 0,$$
 (23)

$$0 \le x_{\min}^j \le x_{\max}^j.$$
<sup>(24)</sup>

Initial conditions:

$$x^{j,1,0,m^{j,1,0}} = 0, (25)$$

$$\phi^{1,1,1,m^{1,1,1}} = 0. \tag{26}$$

In words, the problem (1), subject to (2)–(26), is to find the selling and buying threshold prices per day in a week, for each device type/market, so that the revenue of the entire storage system device is maximized.

#### 213 5. Implementation

In this section we describe the implementation of the model and optimal price thresholds, given by (1)-(26). The technical and economical data on the devices are taken from [11]. All case studies defined by equations were implemented using Matlab<sup>®</sup>.

The problem (1)–(26) could not be solved by standard optimization tech-218 niques, such as gradient-based optimization methods, due to many local 219 minima and even regions in the domain of the yearly benefit function which 220 correspond to the same benefit value. After experimenting with heuristic 221 solution methods, such as particle swarm optimization (PSO), we have ad-222 opted a pattern search (PS) algorithm included in the Matlab optimization 223 toolbox for solving the problem. The main advantages of PS are its speed 224 and the fact that it does not use gradient approximation to maximize the 225 profit function. Therefore, PS is often used for maximizing complicated 226 functionals which are nonsmooth or even discontinuities and/or have many 227 local minima. The method was first proposed in the literature by [25] and 228 is extensively described in [26]. 229

Algorithm for solving the problem (1)–(26) is depicted in Figure 5. For comparison purposes we also calculated the results when using a single weekly set of price thresholds per device, using the algorithm depicted in Figure 6.



Figure 5: Representation of the algorithm solving the problem (1)-(26)





We assume that both devices can be fully discharged  $(x_{j,min} = 0)$  and start discharged  $(x^{j,1,0,m^{j,1,0}} = 0)$ . No self-discharge was considered as the devices are working almost continuously. Ramp rates were also not considered.

#### 238 6. Case studies

#### 239 6.1. Finding optimal price thresholds

We have calculated the solution to the problem (1)-(26) for year 2014 using the pattern search introduced in Section 3. For 2014, the optimal  $u^*$ contains price thresholds depicted in Figure 7.

The generic bulk energy storage power rating is varied between 50 and 243 150 MW for a discharge duration of 5 to 10 hours. The energy rating varies 244 between 500 and 1500 MWh. The power rating is the maximum amount of 245 energy that the device can charge or discharge in one hour. Unless men-246 tioned otherwise, the round trip efficiency is 80% = 0.80, and the charging 247 and discharging efficiencies are equal to  $\sqrt{0.8} \approx 0.8944 = 89.44\%$ ). The 248 electricity market data used to evaluate the profitability of this device is 249 Dutch day-ahead market data provided by the spot market APX-Endex. 250

For the high-power device, the power rating is varied between 20 and 251 60 MW. The nominal discharge duration is of 15 minutes. As energy rating 252 of the device is calculated as its power rating multiplied by its time of dis-253 charge of that same device, the energy rating will vary from 5 to 15 MWh. 254 Therefore, this energy rating interval [5, 15] MWh was selected as the base 255 power rating of device 2. The minimum bid size for the Dutch balancing 256 market is 5 MW [20] per PTU of 15 minutes. The default charging and 257 discharging efficiencies of this device are both 95% (0.95), which results in 258 a round trip efficiency of around 90% (0.90). The balancing market data is 259 publicly available from the Dutch TSO TenneT [28]. The dimensions and ef-260 ficiency levels of both devices are chosen according to technologies described 261 in [11]. Figure 7 shows the solution to the problem (1)–(26) when two sets 262 of thresholds are applied. The size of the bulk and the high power devices 263 in this example are 50 MW, 500 MWh and 20 MW, 5 MWh, respectively. 264 There, different results can be observed for weekdays and weekends. For the 265 day-ahead market and bulk device, weekend thresholds are usually lower. 266 For the balancing market and high power device, the difference is bigger. 267 In this case, the yearly benefit is the highest when the high power device is 268

<sup>269</sup> used to buy less in the weekends and when it sells more during the working days than in the weekends. The last However, it was realized that the im-



Figure 7: Optimal relative thresholds. The value of the selling thresholds indicates how much above the daily mean selling price the electricity will be sold, while the value of the of the buying thresholds indicates how much below the daily mean buying price the electricity will be bought. Device sizes are 50 MW, 500 MWh and 20 MW, 5 MWh, for the bulk and the high power device, respectively. The optimal working day (written as "weekdays" in the caption) buying threshold for the high power device is zero. The yearly benefit with this set of thresholds is 2.615 M€.

270

provement towards a single set of thresholds was limited (0.2 - 1.1%) and 271 the computational time was at least doubled. This is possibly due to the 272 weekend prices being usually lower than the ones of the working days and 273 that their volatility is lower than volatility of the prices for working days. 274 Therefore, less opportunities for the devices to be active in the respective 275 markets. These situations can also be observed in Figure 1 and in Figure 3, 276 particularly for the day-ahead market. Due to this limited improvement of 277 yearly benefit when having variable selling and buying thresholds for work-278 ing days and weekends, we will use the single set of thresholds for the rest 279 of the paper. 280

Using data from 2014, we have calculated the revenues when varying the rating of both devices see Figure 8. Here " $50 \cdot 10$ " refers to a device with a nominal power rating of 50 MW and a discharge duration of 10 h. Increasing the size of the bulk device three times (high power device of 5 MWh, bulk device of 150 MW and 10 h of discharge time) and increasing the size of the high-power device (high power device of 15 MWh, bulk device of 50 MW and 10 h of discharge time) have almost the same impact on the yearly benefit, when compared with the base situation (high power device of 5 MWh, bulk device of 50 MW and 10 h of discharge time). This is an interesting observation for eventual practical applications, as the costs for increasing the size of the two devices can be different. For comparison purposes, we



Figure 8: Yearly benefit when varying the rating of the two devices.

291

have calculated the revenues using only the bulk energy device. The result 292 is shown in Figure 9. Clearly, the power rating has a higher impact on the 293 yearly benefit when compared to the impact of energy rating. The two left 294 bars correspond to the same energy rating (500 MWh) and two different 295 power ratings (50 MW and 100 MW, respectively). Figure 10 shows that 296 the yearly benefit increase when moving from the situation with a single 297 device (Figure 9) to the situation with the dual energy storage system (Fig-298 ure 8). The highest increase of the yearly benefit is for the bulk device 299 with the lowest power and energy rating (50 MW and 500 MWh). With 300 this bulk device, including a high power (HP) device of 5, 10, and 15 MWh 301



Figure 9: Revenues using only the bulk device and data from 2014.

leads to the yearly benefit increase of 85%, 170%, and 256%, respectively. 302 Figure 11 compares the yearly benefits when using only the bulk device and 303 the two devices, respectively, for several device sizes and with price data 304 from 2014. The four subfigures display different yearly benefit distribution 305 between the devices: For the first case (bulk: 100 MW · 10 h, HP: 5 MWh), 306 the bulk device operating on the day-ahead market (device and market 1) 307 obtains 56.03% of the yearly benefit, while the high-power device operat-308 ing on the balancing market (device and market 2) obtains 43.97% of the 309 yearly benefit. The yearly benefit of device 1 is lower than in a stand-alone 310 situation, due to energy transferred from device 1 to device 2. The lower 311 bar shows the yearly benefit when only the bulk device operating in the 312 day-ahead market is used. The comparison of the two bars indicates that 313 by combining devices 1 and 2, the yearly benefit in the day-ahead market is 314 reduced by 20.05%, while the total yearly benefit increases by 42.69%. For 315 the last case (bulk: 50 MW·10 h, HP: 15 MWh), a reduction by 110.95% 316 in the day-ahead market yearly benefit (a net loss of 10.95%) and an in-317 crease of 255.96% in the total yearly benefit can be observed. The results 318 for the examples from figure 11 are shown in table 4. Additionally, we have 319



Figure 10: Revenues increase (in %) from using only the bulk device to two devices.

Bulk	HP	Bulk share	HP share	Bulk variation to	Overall
size	size	(%)	(%)	standalone (%)	increase $(\%)$
100 MW $\cdot 10~\mathrm{h}$	$5 \mathrm{~MWh}$	56.03%	43.97%	-20.05%	42.69%
$50~\mathrm{MW}{\cdot}10~\mathrm{h}$	$5 \mathrm{MWh}$	33.87%	66.13%	-37.26%	85.26%
$50~\mathrm{MW}{\cdot}10~\mathrm{h}$	$10 \ \mathrm{MWh}$	5.93%	94.07%	-83.97%	170.45%
$50~\mathrm{MW}{\cdot}10~\mathrm{h}$	$15 \mathrm{~MWh}$	-3.08%	103.08%	-110.95%	255.96%

Table 4: Results for the examples shown in Figure 11

analysed the impact of round trip efficiency of both devices on the results, see Figure 12. The device ratings are 50 MW and 500 MWh for the bulk device and 20 MW and 5 MWh for the high-power device, respectively. The charging and discharging efficiencies are assumed to be the same and equal to the square root of the round trip energy efficiency. Figure 12 illustrates that the efficiency of the bulk device has a greater impact on the yearly benefit than the efficiency of the high power device.

Furthermore, we have analysed the impact of using energy prices from the years 2012 and 2013 on the model predictions and compared them to those with the 2014 prices. Figure 13 shows the results for a bulk device of



Figure 11: Yearly benefit distribution for the results mentioned in table 4, when using dual and single ESS



Figure 12: Impact on the results of efficiency of the devices. Size of the devices used for the bulk device: 50 MW and 500 MWh, for high power: 20 MW and 5 MWh.

50 MW and 500 MWh and a comparison between the high power devices of 20 MW, 5 MWh and of 40 MW, 10 MWh. Round trip efficiencies are 70% and 90% for the bulk and the high-power devices, respectively. The volatilities towards the previous time slot for the 2012 and 2013 electricity prices are shown in appendix B. The yearly benefit for 2014 are below the average yearly benefit of two years before.

#### 336 6.2. Cost-benefit analysis for different energy storage devices

Here we focus on calculating of the payback period (PBP) for using the ESS, depending on which particular ESS is used. The PBP ( $\psi$ ) is calculated by dividing the initial investment by the yearly net revenues [30] as shown in equation (28). In order to increase the accuracy of this study, we have used



Figure 13: Impact of prices in the revenues. Devices used: Bulk device characteristics are 50 MW, 500 MWh and 70% efficiency. High power efficiency used is 90%, and the ratings used are 20 MW, 5 MWh and 40 MW, 10 MWh.

price data from years 2012, 2013 and 2014. <sup>2</sup> The costs of the devices used to calculate the initial investment are taken from [11]. The costs per unit of power (kW) and unit of energy (kWh) of device j are denoted by  $\mu^j$  and  $\xi^j$ , respectively. The power and energy ratings for a device j are denoted by  $\rho^j$  and  $\epsilon^j$ , respectively. The Euro/Dollar conversion rate is 1/1.10, following the information provided in [27]. The yearly benefit Z(u) is replaced by Z'(u) defined as<sup>3</sup>

$$\sum_{j\in J}\sum_{\delta\in D}\sum_{t_j\in T_j}\sum_{m^{j,\delta,t_j}\in M^j} \left(q_S^{j,\delta,t_j,m^{j,\delta,t_j}} \cdot (p_S^{j,\delta,t_j,m^{j,\delta,t_j}} - \kappa^j) - q_B^{j,\delta,t_j,m^{j,\delta,t_j}} \cdot p_B^{j,\delta,t_j,m^{j,\delta,t_j}} - \kappa^j\right)$$
(27)

<sup>&</sup>lt;sup>2</sup>Other approaches could be used such as the one presented by [29], where energy storage device optimal sizing for arbitrage provision is evaluated.

<sup>&</sup>lt;sup>3</sup>With a slight abuse of notation as u maximizing Z'(u) will differ from original  $u^*$  maximizing Z(u)

which takes the variable the variable O&M costs  $\kappa^{j}$  per unit of energy for device j into account.

The yearly net benefit is calculated by subtracting the yearly operation and maintenance costs  $o^j$  from the optimal yearly benefit  $Z'(u^*)$ . Furthermore, we compare the payback period  $\psi$  defined as

$$\psi = \frac{\sum\limits_{j \in J} (\rho^j \cdot \mu^j + \epsilon^j \cdot \xi^j)}{Z'(u^*) - \sum\limits_{j \in J} o^j}.$$
(28)

for the years 2012–2014 with those of 2014. The internal rate of return  $\iota$  is used to calculate the profitability of potential investments in the ESS and is calculated for a certain prespecified number of years N, so that equality

$$\sum_{n=0}^{N} \frac{Z'(u^*) - \sum_{j \in J} o^j}{(1+\iota)^n} - \sum_{j \in J} (\rho^j \cdot \mu^j + \epsilon^j \cdot \xi^j) = 0$$
(29)

is satisfied. In the two case studies to follow, we will discuss  $\iota$  calculated for N = 10, 15 and 20 years. We will also compare  $\iota$  obtained with average of values for  $Z'(u^*)$  and  $o^j$  over years 2012–2014 with those from 2014 only. As in this case studies we will vary technologies used for the ESS, in Appendix C we discuss technologies available in detail.

6.2.1. Case study 1: Cost benefit analysis with D-CAES and Li-ion battery
 technologies

For the first case study a traditional D-CAES of 50 MW and 500 MWh 346 is used as the bulk device. A Li-ion battery (LI) technology of 10 MWh 347 was selected as the high power device. The round trip efficiencies are 50%348 and 85% for the D-CAES and for the LI, respectively, as reported in [11]. 349 For D-CAES, the minimum costs  $\epsilon^1$  and  $\xi^1$  are  $3.64 \cdot 10^5 \in /MW$  and  $1.82 \cdot 10^5 \in /MW$ 350  $10^3 \in MWh$ , respectively. For LI,  $\epsilon^2$  and  $\xi^2$  are  $1.09 \cdot 10^6 \in MW$  and  $5.45 \cdot$ 351  $10^5 \in MWh$ , respectively [11]. Operation and maintenance costs are the 352 average values presented in [31]. For LI the fixed O&M costs are  $6.9 \in /KW$ -353 yr and the variable costs are  $2.1 \in /MWh$ . For the D-CAES the fixed O&M 354 costs are  $3.9 \in /KW$ -yr and the variable costs are  $3.1 \in /MWh$ . 355

Table 5 shows the results of the cost benefit analysis. The internal rate of return  $\iota$  was calculated for average yearly benefit over years 2012–2014 (see Figure 14 for the yearly benefits and its average) and for 20, 15 and <sup>359</sup> 10 years. The payback period  $\psi$  was calculated for the average yearly benefit <sup>360</sup> from years 2012–2014 and also when the lowest yearly benefit of these 3 years was considered (year 2014). These results show that this system will take



Figure 14: Results for DCAES 50 MW, 500 MWh and 50% efficiency and LI 40 MW, 10 MWh and efficiency 85%.

	Average 2012–2014	2014
$\psi~({ m yr})$	17.30	26.63
$\iota$ at 20 years (%)	1	-3
$\iota$ at 15 years (%)	-2	-6
$\iota$ at 10 years (%)	-9	-15

Table 5: Cost benefit results for case study 1

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more than 17 years to be paid back when considering average year benefits over years 2012–2014. For this case study,  $\iota$  (IRR) in the first 20 years will be slightly positive (1%). Using the values of 2014, it will take almost 27 years for the devices to be paid and  $\iota$  will be negative in all the situations analysed.

### 6.2.2. Case study 2: Cost benefit analysis with AACAES and flywheel tech nologies

For the second case study a AACAES of 50 MW and 500 MWh is used 369 as bulk device, while a flywheel (FW) technology of 15 MWh was selected 370 as a high power device. The round trip efficiencies are 70% and 90% for the 371 AACAES and for the FW, respectively [11]. For AACAES, the costs con-372 sidered are 40% higher than the costs of D-CAES, following [31]. Therefore, 373 the minimum costs  $\mu^1$  and  $\xi^1$  are  $5.09 \cdot 10^5 \in /MW$  and  $2.55 \cdot 10^3 \in /MWh$ , 374 respectively. For FW,  $\mu^2$  and  $\xi^2$  are  $2.27 \cdot 10^5 \in /MW$  and  $9.1 \cdot 10^5 \in /MWh$ , 375 respectively [11]. Operation and maintenance costs are taken from [31]. 376 For FW the fixed O&M costs are  $5.2 \in /KW$ -yr and the variable costs are 377 2.0 euro/MWh. For AACAES, also the fixed O&M costs are increased by 378 40% when compared to D-CAES, to 5.46  $\in$ /KW-yr. For the AACAES vari-379 able costs, as no natural gas is consumed in this case, they are considered 380 the same as for PHES,  $0.22 \in /MWh$ . 381

Table 6 shows the results for the cost benefit analysis. The calculations were performed as in Case study 1. For the assessment of  $\iota$  average yearly benefit over years 2012–2014, depicted in Figure 15, was considered. Parameter  $\iota$  was calculated for N = 20, 15 and 10 years. Two payback periods were calculated with the average yearly benefits over years 2012–2014 first and with only 2014 yearly benefits second. The results demonstrate that

	Average 2012–2014	2014
$\psi$	10.00	14.64
$\iota$ at 20 years (%)	7.72	3
$\iota$ at 15 years (%)	5.53	0.31
$\iota$ at 10 years (%)	0.00	-6.39

Table 6: Cost benefit results for case study 2

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this system will take 10 years to be paid back with the yearly benefit averaged over years 2012–2014. With yearly benefits from year 2014, the system will be bayed back in almost 15 years. With the average yearly benefit,  $\iota$ was positive with N = 10 years, achieving 7.72% around 20 years of usage. For the yearly benefit of 2014,  $\iota$  reaches positive values after 15 years of usage, achieving 3% after 20 years.

The net yearly benefit per kWh of energy sold for both case studies and the three years under analysis are shown in Figure 16. The yearly benefit per KWh is higher in case study 1. However, the amount of energy sold is



Figure 15: Results for AACAES 50 MW, 500 MWh and 70% efficiency and FW 60 MW, 15 MWh and efficiency 90%.

higher in case study 2, as shown in Figure 17. Therefore, the normalized
yearly benefit is higher for case study 2, as can be seen from comparing
Figures 14 and 15.

#### 400 6.3. Discussion

The results obtained in the last two case studies (around 10-27 years of payback time) indicate that systems similar to the ones presented in this paper have, under certain conditions, potential to be cost effective. By varying ratings for the devices used, we could increase yearly benefits by up to 256 %. We have shown how the costs, size and efficiency of the devices impact the feasibility of ESS.

Further integration of variable RES is expected to increase potential revenues from balancing provision. Additionally, with the increasing deploy-



Figure 16: Net yearly benefits for both case studies.



Figure 17: Amounts of energy sold in both case studies.

<sup>409</sup> ment and maturity of energy storage technologies, their investment and <sup>410</sup> maintenance costs are expected to decrease, while their effective life span is <sup>411</sup> expected to increase. This fact, associated with the potential higher volatil-<sup>412</sup> ity of energy prices due to variable RES integration, increases the potential <sup>413</sup> for profitability of systems as the one presented in this paper. Of course, <sup>414</sup> other factors, such as future energy policies, market regulation, price variations and maintenance costs, should be taken into account and optimization
techniques are very useful for assessing the potential profit of the ESS. An
example of a different, but complementary approach, is presented in [29]
where the size of a single device energy storage system is optimized for the
needs of different European markets, comparing two distinct technologies.

The results presented in the case studis, such as the payback period or the 420 internal rate of return may explain why although the ESS can be financially 421 feasible and viable, it has not yet been deployed. The high risk associated 422 with new technologies and business models is another likely reason. Fur-423 thermore, the power system stakeholders are seen as risk-averse, partially 424 due to the need for presenting high levels of reliability, which strengthens 425 the impact of high risk. Finally, there may be other reasons behind the non-426 deployment of these systems and technologies, which should be carefully 427 evaluated. These seem to be of neither technological nor financial nature. 428

#### 429 7. Conclusions

In this paper we presented a novel model of a dual energy storage sys-430 tem using two different storage technologies, trading simultaneously in two 431 energy markets. We have adopted pattern search to find optimal strategies 432 to operate this system. We have analysed the impact of using a dual en-433 ergy storage device system and of different buying and selling strategies for 434 weekdays and weekends. We have shown that it is possible to increase the 435 revenues by up to 270% compared to using a single energy storage device. 436 We have observed that for the price data used no significant improvement 437 was obtained by using different buying and selling strategies for weekdays 438 and weekends. This might change with different price data, though. We 439 have studied impact of size, efficiencies and market price variation on the 440 ESS yearly benefits. Finally, we have demonstrated that, depending on the 441 level of the costs and efficiency of the devices used to build this system, they 442 are be already cost effective. 443

In the framework of an increasing amount of intermittent electricity generation, the price fluctuations in the market are expected to increase, which will then also increase the level of yearly benefits and reduce the payback period of the energy storage systems. Therefore, with the increasing need for electricity network flexibility, the potential of systems like the one presented in this paper is high. Nonetheless, that will depend on many aspects influenced by future decisions and market behaviours, which we cannot take intoconsideration at this stage.

In out future work, we intend to analyse the impact of imperfect price prediction on the economic benefit obtained and more advanced buying/selling
strategies for ESS.

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#### 461 Appendix A: Location of underground salt reservoirs in Europe

Figure 18 shows the location of underground salt reservoirs in Europe. A substantial area of The Netherlands lies above a region where these salt reservoirs are located. These reservoirs can be used to build underground caves which in turn will be part of a compressed air energy storage system (CAES).



Figure 18: Location of underground salt reservoirs in Europe. Courtesy of KBB technologies

# Appendix B: Volatility of the Dutch day-ahead and balancing mar ket for years 2012 and 2013

To calculate the historical price volatility towards the previous time slot 469  $(\sigma_{t_j-t_{j-1}}^{j,\delta,m^{j,\delta,t_j}})$  for market j and day  $\delta$  we used equation (30). Historical price 470 volatility is the standard deviation of price return  $v_{t_j-t_{j-1}}^{j,\delta,t_j}$  calculated by equation (31). In these equations,  $p^{j,\delta,t_j}$  is the spot price at time  $t_j$ ,  $p^{j,\delta,t_{j-1}}$ 471 472 the spot price at time  $t_{j-1}$ ,  $n_{T_j}$  is the number of time periods of the market 473 (24 hours or 96 PTUs) and  $\overline{v}^{j,\delta}$  is the mean of the price quotients  $v_{t_j-t_{j-1}}^{j,\delta,t_j}$  in 474 market j at day  $\delta$ . We have applied equation (30) to the Dutch day-ahead 475 market prices and to both upward and downward prices of the balancing 476 market. For the balancing market, PTU is used instead of the hour which 477 is used in the day-ahead market. 478

$$\sigma_{t_j-t_{j-1}}^{j,\delta} = \sqrt{\sum_{t_j \in T_j} \frac{(v_{t_j-t_{j-1}}^{j,\delta,t_j} - \overline{v}^{j,\delta})^2}{n_{T_j} - 1}}$$
(30)

$$v_{t_j-t_{j-1}}^{j,\delta,t_j,m^{j,\delta,t_j}} = \frac{p^{j,\delta,t_j}}{p^{j,\delta,t_{j-1}}}$$
(31)

In Figures 19 and 20 are presented the volatility towards the previous time slot (hour or ptu) of the Dutch day-ahead and balancing market for the years 2012 and 2013, respectively.



Figure 19: Market volatility towards previous time slot (hour or PTU, depending on the market) for the 2012 day-ahead and balancing market prices.



Figure 20: Market volatility towards previous time slot (hour or PTU, depending on the market) for the 2013 day-ahead and balancing market prices.

# Appendix C: Possible technologies that can be used for energy storage

We have analysed the possible technologies that can be used as bulk and high power technologies, respectively.

For bulk technologies, the available options are: pumped-hydro energy 486 storage (PHES), diabatic compressed air energy storage (D-CAES) and adia-487 batic advanced compressed air energy storage (AACAES). The PHES is 488 widely used and is the most mature bulk technology. However, this tech-489 nology is dependent on geological conditions and availability of possible 490 sites. The geological conditions in The Netherlandsare not optimal to build 491 traditional PHES systems, especially due to the flat landscape. The CAES 492 technologies are appropriate bulk technologies for The Netherlands, as these 493 technologies can be built using either the existing underground salt deposits 494 in the centre and north of the country or the depleted gas reservoirs in the 495 north of the country. See Appendix A for schematic representation of the 496 salt deposits in Europe. The first D-CAES system was installed in 1978 in 497 Germany [11]. This technology uses natural gas to both charge and discharge 498 the underground reservoirs. Although AACAES is currently a theoretical 499 technology, the test results are very promising. Instead of gas-based com-500 pressors, it can use electric compressors. Furthermore, the resulting heat 501 of the air compression which occurs when the device charges is stored and 502 used to heat the expanding air when the device discharges. These AACAES 503 developments increase the efficiency of this technology and reduce operation 504 costs when compared with D-CAES [18]. All bulk technologies have a very 505 long durability of 20-100 years. This includes CAES; the first equipment 506 installed is still functional after 37 years [11]. 507

For the high power energy storage several technologies can be considered 508 [11]. Among those, one may highlight lead-acid, lithium-ion, nickel-cadmium. 509 sodium-sulphur, zebra  $(NaNiCl_2)$  batteries, and flywheels. An appropri-510 ate technology should lead to a very fast response time (in order of few 511 seconds) to any mode switch between charging, idle and discharging. Moreover, 512 such technology should have a modular capacity allowing a realistic imple-513 mentation of the power and energy size specifications of the device. In the 514 long term, another important aspect is the cycling durability, as the high 515 power device will be working very frequently. Lead-acid batteries are a ma-516 ture technology with low initial costs. Lithium-ion batteries present good 517 durability and efficiency. Nickel-cadmium batteries present good durabil-518 ity and robustness to deep discharges. Sodium-sulphur batteries present 519

the advantages of low maintenance and below average initial costs. Zebra  $(NaNiCl_2)$  batteries present good robustness to self discharge. Flywheels have the advantage of a theoretical unlimited amount of charge and discharge cycles.

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